## Supporting information

Table S1: Correlation between target inorganic elements and environmental factors in the sludge.

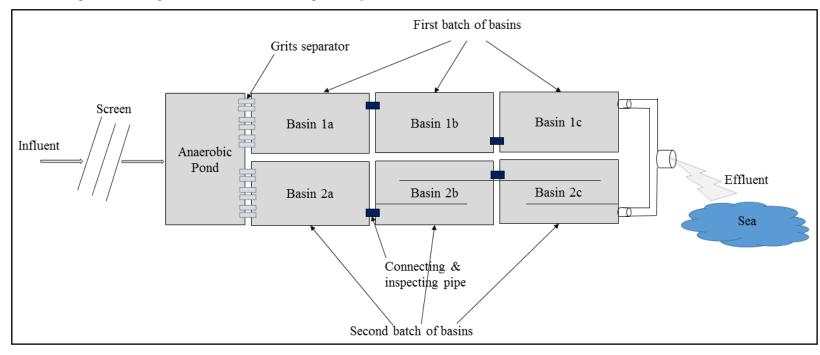
|          |                |   |       |  |  |   |  |  | Sewag             | e sludge    | 2              |              |             |   |                            |               |  |                              |  |   |                             |            |      |                        |           |           |                          |    |
|----------|----------------|---|-------|--|--|---|--|--|-------------------|-------------|----------------|--------------|-------------|---|----------------------------|---------------|--|------------------------------|--|---|-----------------------------|------------|------|------------------------|-----------|-----------|--------------------------|----|
| <u>к</u> | 1.00           |   |       |  |  |   |  | and the  |                   |             |                |              |             |   |                            |               |  |                              |  |   |                             |            |      |                        |           |           |                          |    |
| lg 🛛     | .995           | 1.00  |       |  |  |   |  | Stror  | ig and            | non-sig     | Inificar       | t correl     | ation       |   |                            |               |  |                              | 1.   |   |                             |            |      |                        |           |           |                          |    |
| e        | -0.40          | -0.33   |       |  | -  |   |  | the second s | -                 |             |                | ion at 0.0   |             |   |                            |               |  |                              | 1  | 3   |                             |            |      |                        |           |           |                          |    |
|          | 0.67           | 0.65  | -0.61 | A CONTRACTOR OF A CONTRACTOR A CONT |  | -   |  | Stron  | ig and si         |             |                | on at 0.05   | ilevel      | -   |                            |               | -  |                              | -  |   |                             |            |      | _                      |           |           |                          |    |
|          | 0.27           | 0.27  | -0.53 |  | A CONTRACTOR OF A CONTRACTOR O | and the second se |  |  |                   | No corr     | elatation      | Ř.           | _           |   |                            |               |  |                              |  |   |                             |            |      |                        |           |           |                          |    |
| a        | 0.43           | 0.37  | -0.86 |  | 0.78   |   |  |  |                   |             |                |              |             |   |                            |               | -  |                              |  | <u>.</u>  |                             |            |      | -                      |           |           |                          |    |
| n        |                |   | -0.64 |  | .890   | 0.87  | and the second sec   |  |                   |             |                |              |             |   |                            |               | -  |                              |  |   |                             |            |      |                        |           |           |                          |    |
| In       | .992           | .986  | -0.43 |  | 0.36   |   | -  | 1.00   | 1.00              |             |                | _            |             |   |                            |               |  |                              | ÷  |   |                             |            |      |                        |           |           |                          |    |
| u        | 0.01           | -0.02   | -0.61 |  | .901   | 0.85  | Accession and some   | 0.12   | 1.00              |             |                | _            |             | -   |                            |               | -  |                              | -  |   |                             |            |      |                        |           |           |                          | _  |
|          | .965           | .949  | -0.53 |  | 0.48   | -   |  |  | 0.27              | 1           | 1.00           |              |             |   |                            |               | -  | -                            | -  |   |                             |            |      |                        |           |           |                          |    |
| a        | 0.48           | 0.43  | -0.78 |  | 0.88   | and the second second   | .892   |  |                   |             |                |              |             | -   |                            |               | -  | _                            | -  |   |                             |            |      |                        |           |           |                          |    |
| 2        | -0.80<br>-0.77 | -0.76   | 0.71  | -0.43  |  | -0.46   |  | -0.76  |                   | -0.76       |                | 1.00<br>0.73 | 1.00        |   |                            |               |  |                              |  | <u>i</u>  |                             |            |      |                        |           |           |                          |    |
| r<br>b   | 0.17           | 0.15  | -0.67 |  | CONTRACTOR OF THE OWNER   |   |  | -0.82<br>0.26  |                   | 897         |                | -0.15        |             | -   |                            |               |  |                              | -  |   |                             |            |      |                        |           |           |                          | _  |
|          | 0.11           | 0.15  | -0.60 |  | .969 <sup>°°</sup><br>0.87   | 0.83  |  | 0.20   | .944              | 0.33        |                | -0.15        | -0.85       | and the second second   | _                          |               |  |                              |  |   |                             |            |      |                        |           |           |                          | _  |
| Ь        | 0.01           | 0.00  | -0.42 | 1.000.000  |  | 0.75  |  | 0.12   |                   | 0.05        |                |              |             |   | 0.69                       | 1.00          | 1  | -                            |  |   |                             |            |      |                        |           |           |                          | _  |
| 0        | 0.07           | 0.00  | -0.42 |  | .933   |   |  | 0.12   | STORE STORE STORE | 0.20        |                | -0.23        | -0.40       |   | 0.63                       |               |  | -                            |  |   |                             |            |      |                        |           |           |                          |    |
| 0        | -0.18          | -0.21   | -0.56 |  | 0.82   | 1.00 100  | .949   | -0.07  | .939 <sup>°</sup> | 0.01        |                |              | -0.43       |   | 0.03                       |               |  | -                            | -  |   |                             |            |      |                        |           |           |                          |    |
| -        | -0.18          | -0.21   | -0.34 |  | 0.84   | 0.65  | A CONTRACTOR OF  | -0.07  |                   | 0.00        |                |              | -0.43       |   | 0.50                       |               | .926   | 964                          |  |   |                             |            |      |                        |           |           |                          |    |
| 0        | -0.23          |   |       | - 964  | -0.72  |   |  |  | .948              |             |                |              |             |   | and the second second      | .971          | -0.51  | and the second second second | and the second |   |                             |            |      |                        |           |           |                          |    |
| s<br>d   | 0.04           | -0.83<br>0.02   | -0.66 |  |  |   | -0.55  | 897  |                   | 948<br>0.28 | -0.85          |              | .912        | The second s  | 962 <sup>***</sup><br>0.71 |               |  |                              |  | and the second se | 1.00                        |            |      | -                      |           |           |                          |    |
|          | 0.04           | 0.02  | -0.00 |  | .937   |   | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  | 0.14   |                   | 0.20        |                | -0.08        | -0.55       | Contract of the   | 0.70                       | .000          | .945   | .947                         | 10000  |   |                             | 1.00       | -    |                        |           |           | 1                        | _  |
| +        | -0.66          | -0.68   | -0.26 |  | .897   | .901<br>-0.08   | .989   | -0.68  | .985<br>0.08      | 1.000       | .910<br>-0.19  |              | 0.36        | .964 <sup>***</sup><br>0.10   |                            | .921<br>-0.06 | 0.27   | .958                         |  |   | .982 <sup>***</sup><br>0.18 |            | 1.00 | -                      |           |           |                          |    |
| ,<br>C   | -0.61          | -0.57   | .903  |  |  | 923   |  |  |                   | -0.76       |                | 0.68         | .918        |   | 883                        |               |  |                              |  | 0.84  |                             |            | 0.06 |                        | -         |           |                          |    |
|          | 0.07           | 0.04  | -0.72 |  | .922   | 0.85  | And in case of the local division of the loc | 0.16   |                   |             | 0.87           |              |             | .988  |                            |               | .962   | and the second second        |  |   | .997                        |            | 0.21 | Annual State of States | 1.00      |           |                          |    |
|          | 0.43           | 0.39  | -0.81 |  | .322   | 974   | .909"  | 0.51   | .898              | 1000000     | .994           | -0.40        |             | the second se | 0.88                       | 0.83          | Statement of the local division in the local division of the local | 0.81                         |  |   |                             |            |      | 940                    | .914      | 1.00      | -                        |    |
|          | 0.45           | 0.06  | -0.68 |  | .034   | 0.86  | STREET, STREET | 0.19   |                   | 0.33        |                | -0.10        |             | Contraction of the second   | 0.73                       | .941          |  | .949                         |  |   | .000                        | .992       |      | -0.79                  |           | .926      | 1.00                     |    |
| M        | 0.00           | 0.19  | -0.71 |  | .956   |   | Contraction of the local distance  | 0.29   | .929              | 0.43        | a state of the |              | -0.64       |   | 0.81                       |               |  |                              |  | -0.66   |                             | .958       | 0.14 |                        |           | .933      | .981"                    | 1  |
|          |                |   | Fe    | AI   | .364<br>K  | Ba  | .925<br>Zn   |  | .929<br>Cu        | 0.40<br>Sr  | .836<br>Ga     | -0.21<br>V   | -0.04<br>Cr | .998<br>Pb  | Rb                         | .836<br>Ni    | .920 <sup>°</sup><br>Mo  | V.01                         | Co   | -0.00<br>As   | .982<br>Cd                  | .958<br>Ti | oH   | EC                     | .385<br>C | .933<br>N | NOV THE REAL PROPERTY OF | OM |
|          | relation is si |   |       |  |  | Ua  |  | 111  | cu                | 015         | 0a             | ¥.           | u .         | PD.   | HD.                        | nal 2         | no   |                              | 00   | HS  | Cu                          |            | pri  | 20                     | 0         | TN .      | 5                        | OP |
|          | elation is sig | and the second se |       |  |  |   |  |  |                   |             |                |              |             |   |                            |               |  |                              |  |   |                             |            |      |                        |           |           |                          |    |
| 1        |                |   |       |  |  |   |  |  |                   |             |                |              |             | 1   |                            |               |  | 1                            |  |   |                             |            |      |                        |           |           |                          |    |

Table S2: Correlation between target inorganic elements and environmental factors in the sediment.

| Þ        | 1.00           |              |          |             |       |       |       |      |       | Bedimen              | t   | _        |         |         |      |       |          |      |         |       |       |       |       |       |   |      |      | _    |
|----------|----------------|--------------|----------|-------------|-------|-------|-------|------|-------|----------------------|---|----------|---------|---------|------|-------|----------|------|---------|-------|-------|-------|-------|-------|---|------|------|------|
| Р<br>Mg  | 1.00<br>.825   | 1.00         |          |             |       |       |       |      | Strar | a and                | non-sig   | nifianni | norrol  | tion    |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
| Fe       | 0.72           | .949""       | 1.00     |             |       |       |       | -    |       | -                    | gnificant   |          |         |         | -    |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| AL       | .966           | .862         | 0.80     | 1.00        |       |       |       | -    |       |                      | gnificant (   |          |         |         |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
|          | 0.60           | .905         | .979"    | 0.72        | 1.00  |       |       |      | JUDI  | iyanusi              | No corre  |          | mato.oc | level   |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
| n<br>Ba  | 0.68           | 0.23         | 0.01     | 0.52        | -0.16 |       |       |      |       |                      | NOCORE  | atation  | -       | _       |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| Da<br>Zn | .932           | 0.23         | 0.50     | .838        | 0.34  |       | 1.00  |      |       |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| Mn       | 0.75           | .983         | .985     | .817        | .968  | 0.06  | 0.54  | 1.00 |       |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   | -    | -    |      |
| Cu       | 0.72           | 0.28         | 0.09     | 0.57        |       |       | .897  | 0.12 | 1.00  |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
| Sr Sr    | .850           | .981         | .974     | .904        | .924  | 0.22  | 0.67  |      | 0.29  | 1.00                 |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   | -    | -    |      |
| Ga       | 0.68           | 0.23         | 0.02     | 0.53        | -0.16 |       | .871  | 0.07 | .991" | 0.23                 | 1.00  |          |         |         |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| v        | 0.70           | .948         | .998     | 0.79        | .987  | -0.02 | 0.47  |      | 0.05  |                      | -0.02   | 1.00     |         |         |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| Ċr       | 0.76           | .965         | .995     | .842        | 970   | 0.07  | 0.55  |      | 0.14  | .988"                | 0.07  | .995     | 1.00    |         |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
| РЬ       | .864           | 0.54         | 0.33     | 0.73        | 0.16  |       | .974  | 0.39 | .949  | 0.52                 | .944  | 0.29     | 0.38    | 1.00    |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| RЬ       | 0.75           | 941"         | .980     | .856        | .972  | 0.04  | 0.51  |      |       | .973                 | 0.04  | _        | .989    | 0.34    |      |       |          |      |         |       |       |       |       |       |   | -    |      |      |
| Ni       | .979           | .911         | .828     | .985**      | 0.73  | 0.55  | .877  | .854 | 0.59  |                      | 0.55  | .812     | .865    | 0.77    | .857 | 1.00  | 2        |      |         |       |       |       |       |       |   |      | -    |      |
| Мо       | .971           | 0.78         | 0.65     | .926**      | 0.51  | 0.76  | .978" | 0.68 | 0.80  | of the second second | 0.76  | 0.63     | 0.70    | .910    | 0.67 | .952" | 1.00     |      |         |       |       |       |       |       |   |      |      |      |
| Y        | .820           | .988         | .954 *** | .883        | .929  | 0.18  | 0.63  | .985 | 0.22  | .980                 | 0.19  | .954     | .971    | 0.49    | .970 | .909  | 0.75     | 1.00 |         |       |       |       |       |       |   |      |      |      |
| Co       | .950           | 0.67         | 0.50     | .861        | 0.35  | .869  | .994  | 0.54 | .893  | 0.67                 | .871  | 0.47     | 0.55    | .975 ** | 0.52 | .888  | .974 *** | 0.64 | 1.00    |       |       |       |       |       |   |      |      |      |
| As       | 0.59           | .897"        | .982     | 0.69        | .995  | -0.17 | 0.33  | .961 | -0.10 | .918                 | -0.17   | .986 **  | .966 ** | 0.15    | .957 | 0.71  | 0.49     | .910 | 0.33    | 1.00  |       |       |       |       |   |      |      |      |
| Cd       | .955           | .950**       | .871     | .966**      | 0.78  | 0.48  | .846  | .900 | 0.53  | .959"                | 0.49  | .859"    | .904    | 0.73    | .888 | .994  | .930     | .942 | .851    | 0.77  | 1.00  |       |       |       |   |      |      |      |
| TI       | .985           | 0.76         | 0.61     | .921"       | 0.47  | 0.79  | .977" | 0.65 | .819  | 0.76                 | 0.79  | 0.58     | 0.66    | .937    | 0.64 | .943  | .984     | 0.74 | .989"   | 0.45  | .912  | 1.00  |       |       |   |      |      |      |
| pН       | 0.18           | 0.28         | 0.44     | 0.29        | 0.40  | -0.12 | 0.14  | 0.34 | -0.01 | 0.40                 | -0.12   | 0.45     | 0.44    | -0.05   | 0.39 | 0.27  | 0.25     | 0.25 | 0.08    | 0.43  | 0.29  | 0.11  | 1.00  |       |   |      |      |      |
| EC       | -0.55          |              | 885"     | -0.61       | 881   | 0.04  | -0.43 | .924 | -0.01 | 861                  | 0.04  | 900"     |         | -0.27   | 836  | -0.69 | -0.55    | 877  | -0.39   | 884   | -0.76 | -0.48 | -0.35 | 1.00  |   |      |      |      |
| С        | 0.79           | 0.37         | 0.17     | 0.65        | -0.01 | .987  | .931  | 0.22 | .988  | 0.37                 | .987"   | 0.13     | 0.22    | .978    | 0.20 | 0.67  | .847     | 0.33 | .936 ** | -0.02 | 0.61  | .878  | -0.06 | -0.08 | 1.00  |      |      |      |
| N        | 0.76           | 0.33         | 0.12     | 0.61        | -0.06 |       | .912  | 0.17 | .992  | 0.32                 | .993  | 0.08     | 0.17    | .970    | 0.14 | 0.63  | .816     | 0.28 | .917    | -0.06 | 0.57  | .852  | -0.09 | -0.04 | .998  | 1.00 | 1.00 |      |
| S        | 0.68           | 0.19         | -0.02    | 0.56        | -0.17 |       | 0.81  | 0.04 | .933" | 0.20                 |   | -0.05    | 0.05    | .892    | 0.06 | 0.54  | 0.72     | 0.18 | .836    | -0.20 | 0.46  | 0.77  | -0.22 | 0.14  | and the second se | .955 | 1.00 | 1.00 |
| OM       | 0.80           | 0.39         | 0.18     | 0.66        | 0.01  | .984  | .939" | 0.23 | .988  | 0.39                 | and the second se | 0.15     | 0.24    | .977"   | 0.21 | 0.69  | .860     | 0.34 | .941"   | 0.00  |       | .883  | -0.02 | -0,10 | and the second second   | .994 | .948 | 1.0  |
|          |                |              | Fe       | Al          | K     | Ba    | Zn    | Mn   | Cu    | Sr                   | Ga  | V        | Cr      | РЬ      | RЬ   | Ni    | Mo       | Y    | Co      | As    | Cd    | TI    | pН    | EC    | С   | N    | S    | OM   |
|          | relation is s  |              |          |             |       |       |       |      |       |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
| .Corre   | elation is sig | gnificant at | 0.05 lev | el (bilater | al).  |       |       |      |       |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   |      |      |      |
|          |                |              |          |             |       |       |       |      |       |                      |   |          |         |         |      |       |          |      |         |       |       |       |       |       |   |      |      |      |

## Wastewater and sludge treatment facility.

The only treatment plant for wastewater from Cotonou and surrounding areas (Sèmè-Kpodji and Abomey-Calavi) consists of two series of three waste stabilization ponds receiving effluent from an anaerobic pond (Fig. S1).



## Fig. S1: Schematic diagram of the WWTP Treatment plant.

**Description**: It consists of a system of aerated basins set up to treat and improve the physical and biological properties of the wastewater. Specifically, two series of three stabilization basins (aerated basins) receiving each effluent from an anaerobic pond, can be identified in the treatment facility. The anaerobic ponds, is used for sanitation and degradation of organic matter, the stabilization basins are used for (i) the removal of BOD and pathogens and (ii) the maturation of the sludge (which consists in effectively reducing the population of fecal bacteria).